

Appendix E

GEO-TECHNICAL SERVICES
Consulting Engineers & Geologists

JOB CATAWISSA CREEK

SHEET NO. _____ OF _____

CALCULATED BY SJM DATE 11/81

CHECKED BY _____ DATE _____

~~DATE~~ ONIEDA TUNNEL

HYDROLOGY

E1 - E4

DOWNFLOW BED DESIGN

E5 - E6

DRUM DESIGN

E7 - E9

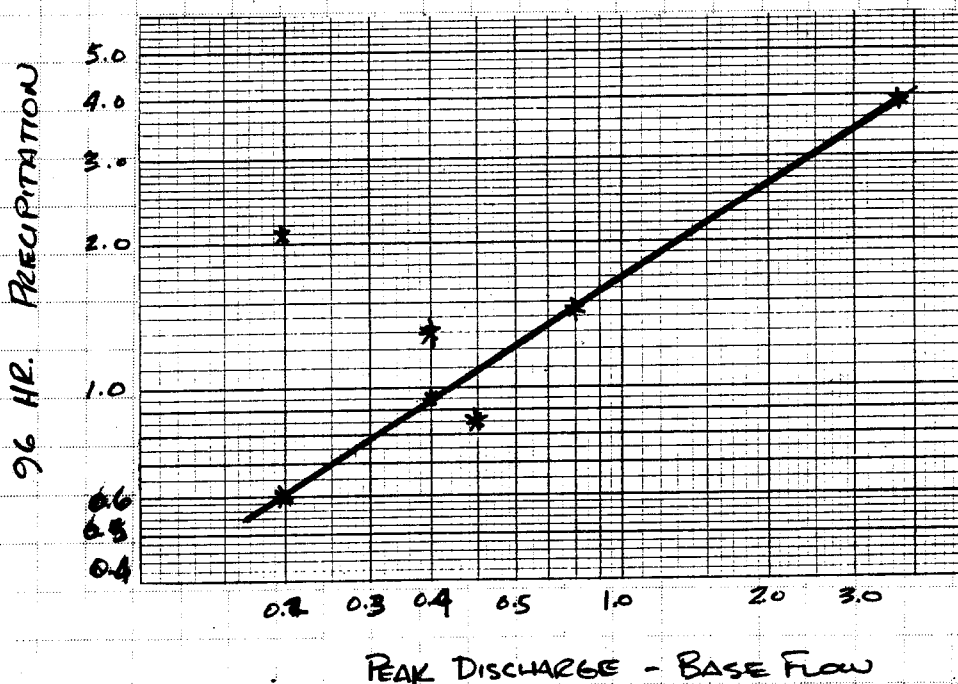
LIMESTONE USAGE

E10

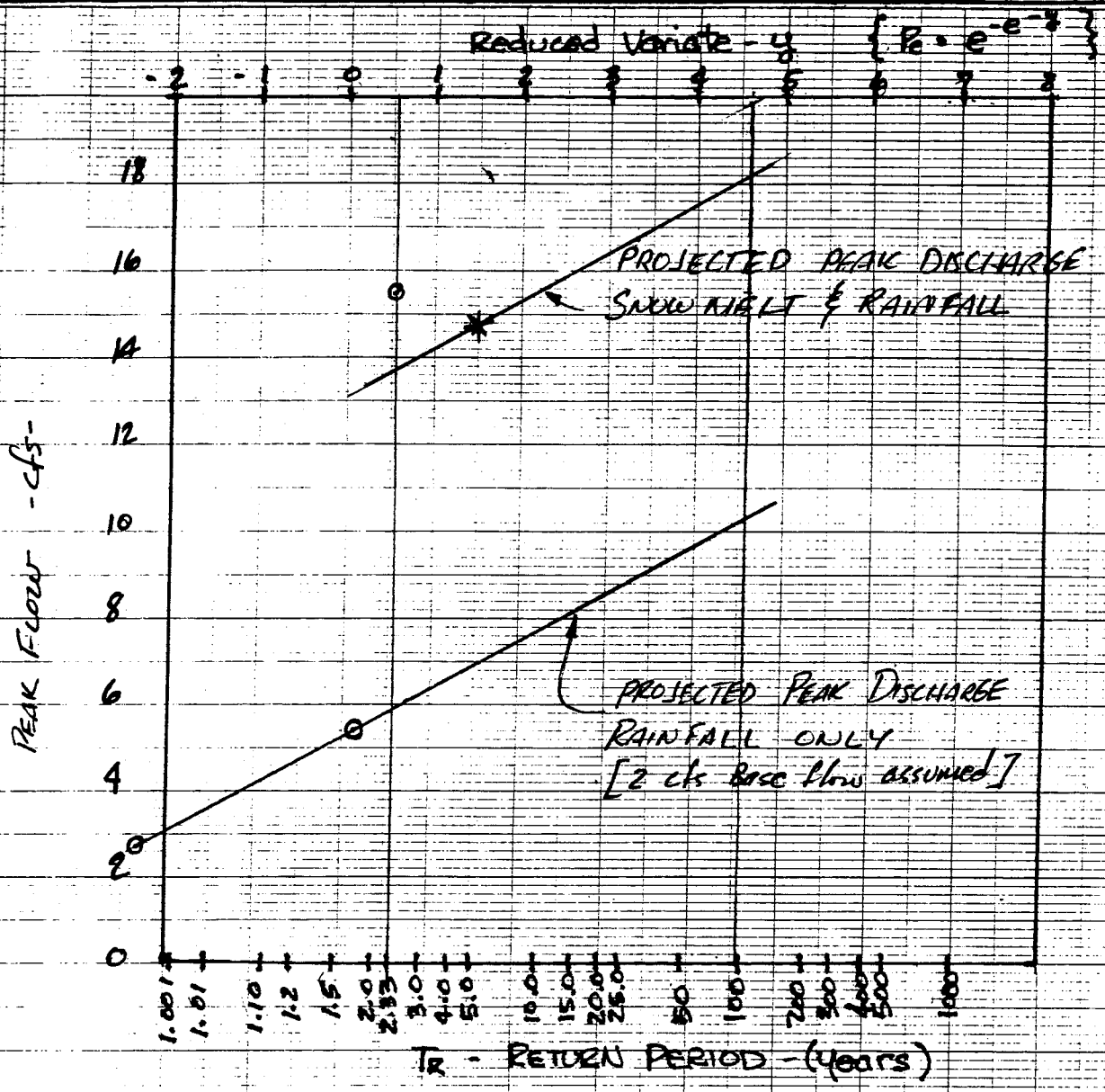
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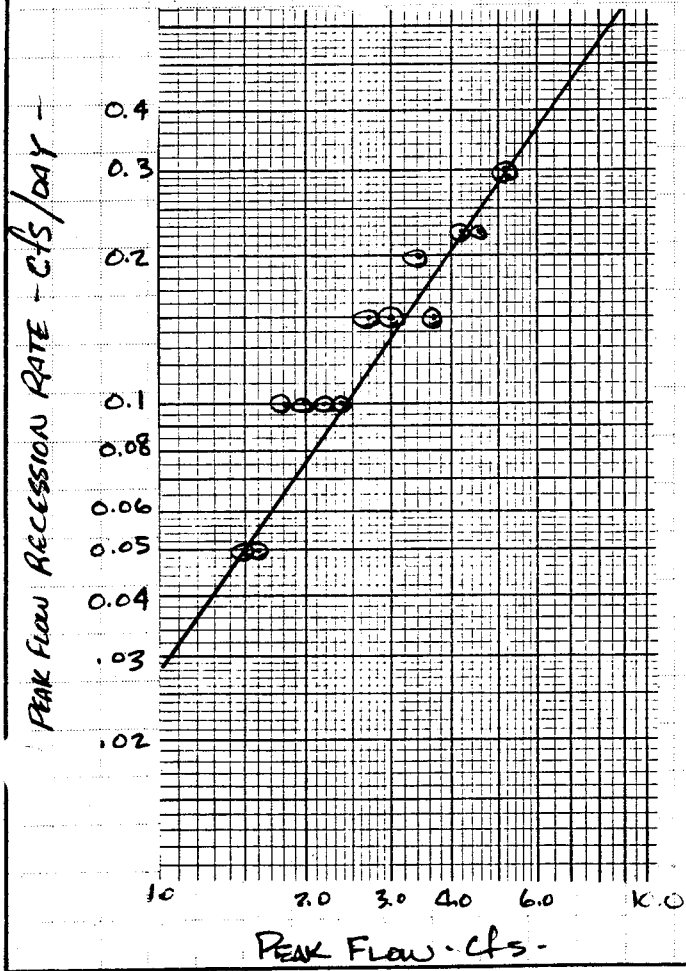
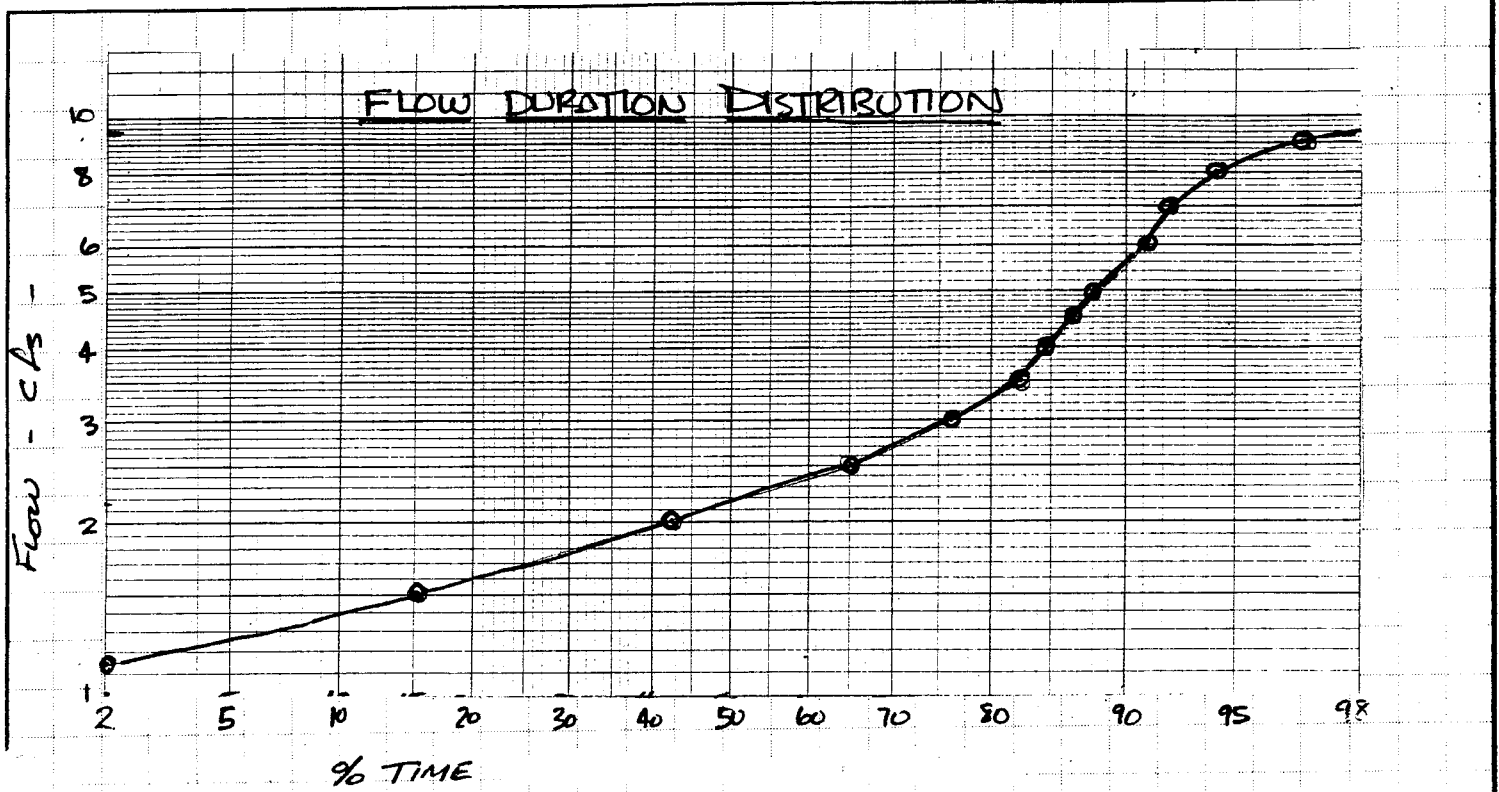
HYDROGRAPH EVALUATION

DATE	Q _P	Q _B	ΔQ	PRECIP (inch)	LAG TIME (HR)	96 HR PRECIP	REMARKS
	cfs						
1) 3/23	2.9	2.5	0.4	0.95	60	0.95	24 hr. storm
2) 5/23	5.5	1.8	3.7	2.60	74	3.95	44 hr. "
3) 4/27	2.4	2.0	0.4	1.00	70	1.30	5 hr. "
4) 4/13	2.5	2.3	0.2	0.45	81	0.60	6 hr. (snow melt.?)
8/12				0.35			
5) 8/13	2.5	2.0	0.5	0.50	46	0.85	8 & 18 hr.
6) 8/25	2.0	1.8	0.2	0.90	11	2.1	1/2 hr. (localized.?)
7) 9/19	2.0	1.2	0.8	1.20	15	1.45	9 hr.



OBSERVED PEAK = 14.8 CF 1/24/79 TR = 5yr





SET :

DESIGN FLOW - 10 cfs
 MAX TREATMENT - 20 cfs
 EMERGENCY BYPASS - 30 cfs

JOB CATAWISSA CREEK

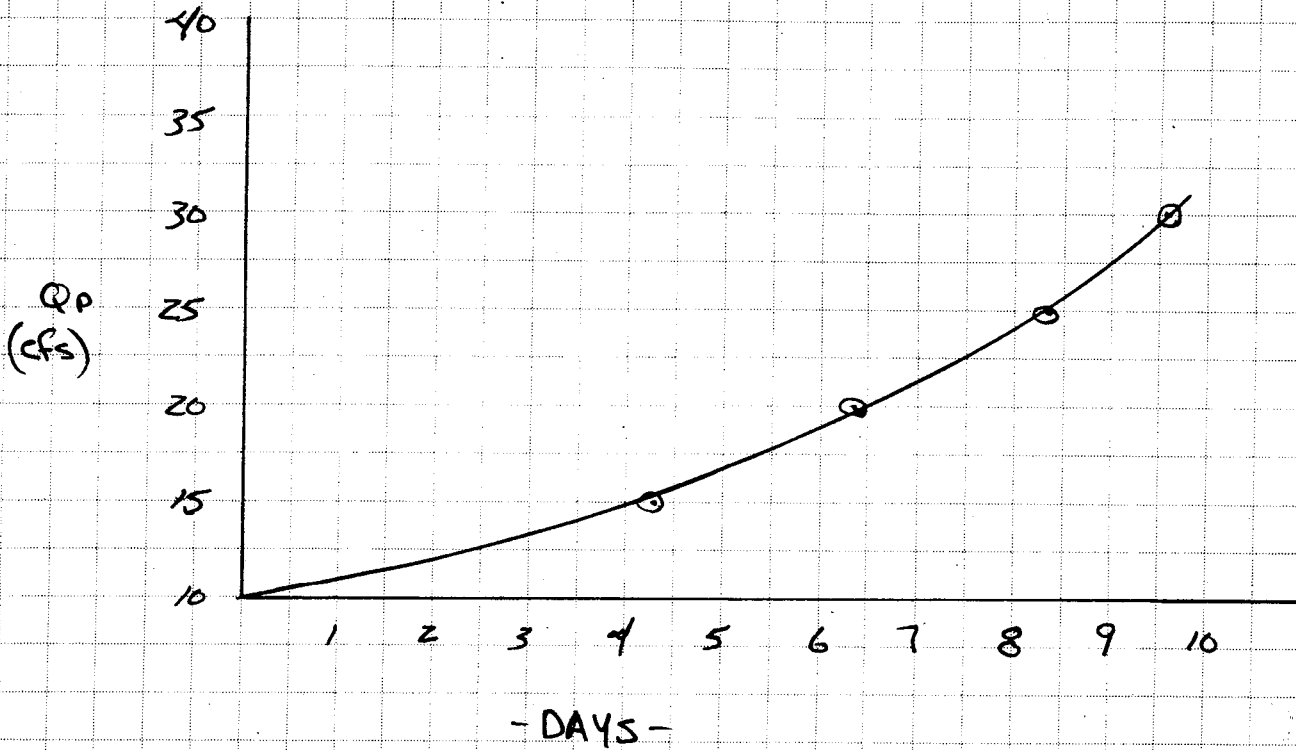
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Consulting Engineers & Geologists

SHEET NO. _____ OF _____

CALCULATED BY TG DATE 10/19

CHECKED BY _____ DATE _____

~~SOURCE~~ ONIEDA TUNNEL



TIME DURATION FLOW EXCEEDS DESIGN FLOW (10 cfs)

ONIEDA TREATMENT DESIGN

CHEMICAL PARAMETERS FOR TREATMENT DESIGN

Flow -cfs-	pH	ACIDITY -mg/l.	ALK # mg/l	CT #	
1	3.30	150	-50	100	* ESTIMATED FROM EQUILIBRIUM CONDITIONS
2	3.50	140	-40	100	
4	3.60	110	-26	84	
6	3.62	90	-24	66	
10	3.65	80	-22	58	
20	3.70	70	-20	50	

STATIC BED - REQUIRED LOAD FACTORS R = 0.5

Flow	pH				
	5.0	5.25	5.5	5.75	6.0
1	34	64	152	380	1160
2	31	58	140	360	1120
4	30	53	120	320	880
6	28	46	104	240	800
10	27	44	92	226	640
20	26	42	88	216	520

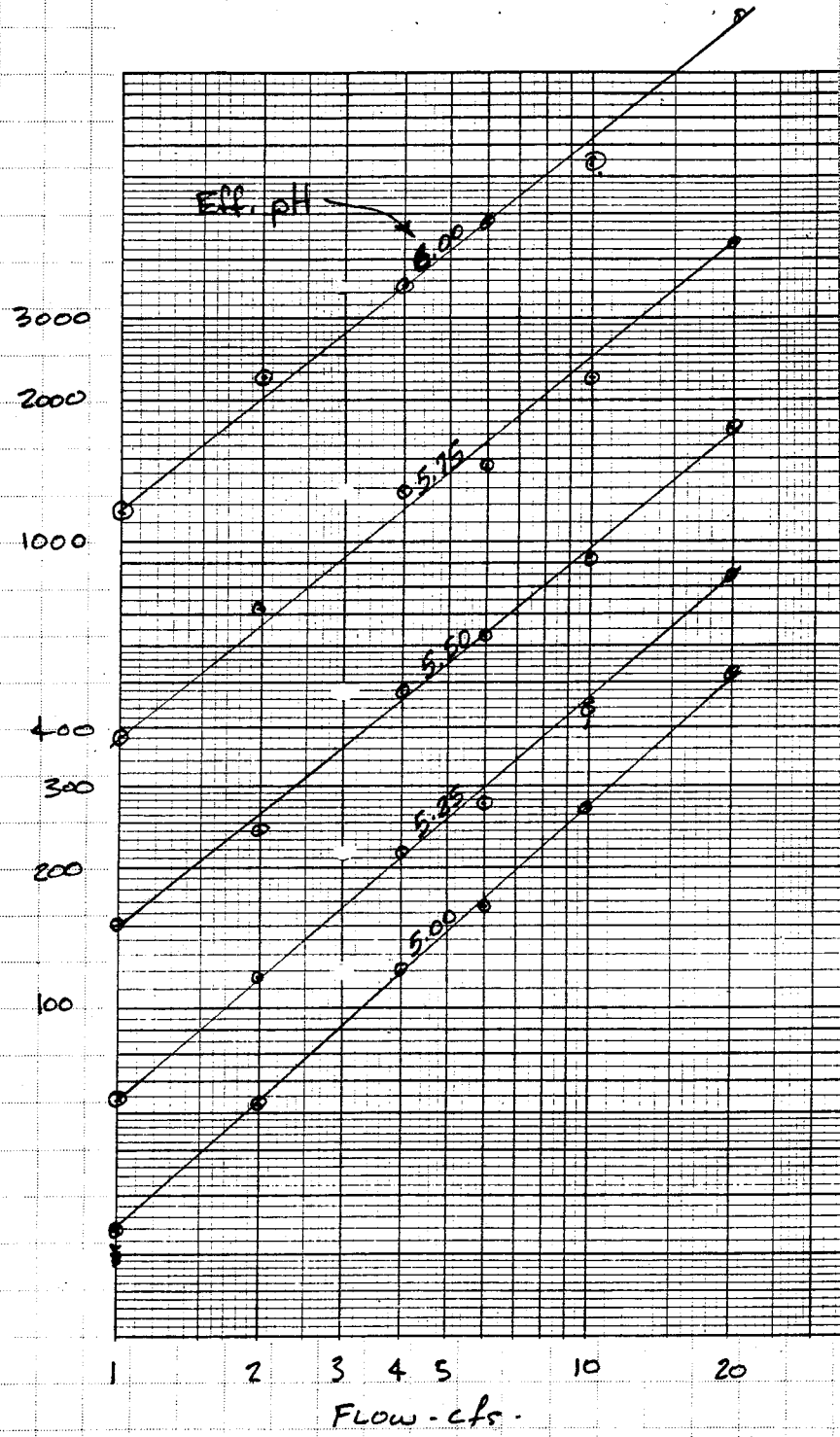
(From Rpt. Table)

[PLOT NEXT SHEET]

REQUIRED STONE AREA = SAME AS DETERMINED = $2 \cdot Q \cdot LF$

ONIEDA TUNNEL

REQ'D AREA (sf.) OF DOWN FLOW BED 5' DEEP



ESTIMATE REQUIRED HEADS FOR DRUM TREATMENT

DRUMS ALONE

Q	Δ ALK	H
1	90	23
2	80	21
4	66	17
6	64	16
10	62	16
20	60	15

DRUMS & 1000 SF DOWNFLOW

Q	Δ ALK	H	pH
1	20	5.1	5.95
2	18	5.6	5.85
4	16	6.2	5.70
6	13	7.0	5.60
10	12	7.2	5.55
20	10	7.7	5.30

} BED EFFLUENT

DRUMS & 2000 SF DOWNFLOW

Q	Δ ALK	H	pH
1	25	3.8	6.1
2	22	4.6	6.0
4	20	5.1	5.95
6	17	5.3	5.80
10	16	6.2	5.70
20	12	7.2	5.6

ASSUMES REQ'D ALK @ pH = 6.5 = 40 mg/l
 $H = \frac{\Delta \text{alk}}{0.13 \text{ (L/gal)}}$

DESIGN

USE : 2000 SF DOWNFLOW BEDS
1000 SF REDUNDANT SYSTEM *
w/ 2 DRUM TIERS

PROPORTION BACKWASH FLOW BASED ON APPROXIMATED
VOLUME = $\frac{2000}{5000} \times 100,267 = 40,100 \text{ CF}$
provide 2x

* is system to work w/ 1/2 Bed & 2 SETS OF DRUMS
OR FULL BED & 1 DRUM

SET OPT. CRITERIA - DRUM TO WORK AT 1 CFS

TRY $G \phi = KD$
 $D = 4'$
 $L = 2'$

$$P_{in} = .67 (1) (6) \times 2 = 502 \text{ ft-lb./SEC}$$

$$M_r = 580 \text{ ft-lb/ft (Ref. Fig. 57)}$$

$$\frac{M_r}{L} = 614.4$$

$$L = 2$$

$$\text{Clz. RPM : } \text{RPM} = \frac{60}{2\pi} \times \frac{P_i}{L} \times \frac{1}{M_r} = 3.9 \text{ RPM}$$

GRINDING RATE @ 3.9 RPM $\approx 4.5 \text{ lbs/HR./ft}$

$$\text{REQ'D RATE} = U_R = .33 \Delta k Q$$

$U_R = 30 \text{ lbs/HR}$	no beds
$= 6.6 \text{ lbs/HR}$	1 bed.
$= 5.0 \text{ lbs/HR}$	2 beds

PRODUCTION RATE = 9 lbs/HR for L = 2'

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CHECK OPERATION AT 2 cfs.

$RPM = 7.8$

PRODUCTION = $E_T \frac{23.5}{550} P_2$ $E_T = \frac{470}{580} = .81$

$U = 17.4 \text{ lbs/HR PER DRUM (34.8 TOTAL)}$

$U_R = 53 \text{ w/ no beds} > 34.8$

$= 14.5 \text{ lbs/HR w/ 1000 sf.} < 17.4$

$= 11.9 \text{ lbs/HR w/ 2000 sf} < 17.4$

CHECK OTHER FLOWS

Q	REQ'D PRODUCTION			PRODUCTION	
	NO BED	1000' BED	2000' BED	1 DRUM	2 DRUMS (6'φ x 2)
1	30	7	5	9	18
2	53	15	12	17.4	35
4	87	52	27	33	66
6	127	53	46	~	~
8	161	71	64	~	~
10	205	92	80	~	~
20	396	198	168	~	~

↖ 2 - 6'φ x 2 DRUMS WILL TREAT BETWEEN 6' & 8 cfs

TRY ADDITIONAL DRUMS 6'φ x 4' FOR HIGH FLOWS

RUN ON EXCESS FLOW ABOVE 4 cfs

Q	U (1 drum)	TOTAL PRODUCTION (4 DRUMS - 2 small)
6	- 0 -	66
8	25	116 (91)
10	50	166 (116)
12	63	192 (129)

2 small & 1 large
2nd large drum
could be set to run
at flows > 12 cfs

ANNUAL LIMESTONE USE :

DURATION %	DAYS /yr	FLOW cfs	- DRUMS -		- DOWNFLOW -		TOTAL TONS
			FINES lbs/hr.	TOT. FINES lbs	ACID mg/l	LBS NEUT. lbs	
0-2	7.2	1	18	3110	150	3201	3.2
2-5	11	1.2	22	5808	148	5265	5.5
5-10	18.3	1.3	25	10980	147	10367	10.7
10-20	36.5	1.5	27	23652	145	23535	23.6
20-30	36.5	1.7	31	27156	143	26305	26.7
30-40	36.5	1.9	35	30660	140	28783	29.7
40-50	36.5	2.1	37	32412	138	31358	31.9
50-60	36.5	2.3	42	36792	134	33349	35.1
60-70	36.5	2.6	46	40296	131	36855	38.6
70-80	36.5	3.0	51	44676	125	40576	42.6
80-90	36.5	5.0	66	57816	100	54103	56.0
90-95	18.3	7.0	91	39967	86	32657	36.3
95-98	11	9.0	141	37224	83	24360	30.8
98-100	7.2	30 ^(USE 20)	192	33178	70	29883	31.5

ANNUAL LIMESTONE CONSUMPTION (TONS) 402.2

USE RATE FORMULAS *

DRUMS TOT. FINES:

$$\text{TOTAL FINES} = \text{FINES (lbs/hr)} \times 24 \text{ hr/day} \times \text{days}$$

DOWNFLOW LBS. NEUT.:

$$\text{LBS. ACID NEUTRALIZED} = 1.1 \left[\frac{\text{ACIDITY}^{**} (\text{mg/l}) \times \text{FLOW (cfs)} \times 5.3901 \times \text{days}}{2} \right]$$

* Developed from experimental results at Quakake.
** Assumes Complete Acid Removal (conservative limestone use estimate)